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"ELECTRIFIED VACUUM PANEL"

The present invention relates to an electrified vacuum panel, and in particular a vacuum panel comprising rheophores for powering electric or electronic devices arranged therein, as for example a sensor for measuring the vacuum.

It is known that the quality of vacuum panels depends upon the vacuum degree inside them, so that it is necessary, during the manufacture, to measure the pressure of the residual gases in several samples for evaluating their quality. The methods employed for this measurement use invasive devices and are generally carried out manually in laboratory, with following high costs and long duration. Moreover, because of its sampling nature, this quality control cannot exclude a single failure in a series of vacuum panels.

The object of the present invention is therefore to provide a vacuum panel free from these drawbacks, that is a vacuum panel wherein the vacuum degree can be controlled in short times and without tamperings. Said object is achieved with a vacuum panel, the main features of which are specified in claim 1, while other features are specified in the following claims.

Thanks to the particular electrification thereof, the panel according to the present invention can permanently house a sensor for carrying out quick and accurate measurements of the residual gas pressure.

Through this arrangement it is possible to determine rapidly and accurately the quality of the vacuum panels not only during their manufacture, but also after a long time from their installation, or periodically, so as to accomplish a continuous check.

Furthermore, the conductive bands used for the electrification can be easily manufactured and assembled together with the vacuum panels, since they are preferably made up with the same material used for the relevant barrier sheets, or with a material similar or compatible with the latter.

Further advantages and features of the vacuum panel according to the present invention will be clear to those skilled in the art from the following

detailed and non-limiting description of one embodiment thereof with reference to the attached drawings wherein:

- figure 1 shows a partial cross-sectional top view of the vacuum panel according to this embodiment of the invention;

5 - figure 2 shows an enlarged partial sectional view taken along plane II-II of the vacuum panel of figure 1; and

- figures 3 and 4 show two working diagrams of a pressure sensor arranged in the vacuum panel of figure 1.

Referring to figure 1, the vacuum panel according to the present
10 embodiment of the invention includes internally a pressure sensor comprising a housing 1 preferably cylindrical-shaped, inside which a wire 2 of conductive material is arranged. The internal volume of housing 1 is much greater than the volume of wire 2; in particular, the internal diameter d_1 of housing 1 is much greater than diameter d_2 of wire 2, that is, $d_1 \gg d_2$. The interior of housing 1 is
15 suitably connected to the interior of the vacuum panel so as to exchange gases with it. In particular, housing 1 is gas permeable and can be formed of a tube of a non-porous material, for example glass, which is provided of a plurality of holes, or of a tube of a porous material, for example ceramic or alumina. Wire 2 is preferably made up of nickel, platinum or tungsten, that is metals having a high
20 temperature coefficient α_T of the resistance and a low emissivity ϵ_r . The ends of housing 1 are provided with two closing elements 3, 3', for example substantially conical- or frustoconical-shaped. The external ends of the closing elements 3, 3' are in turn crossed by two conductive terminals 4, 4', in which are inserted the ends of wire 2, which is therefore taut in the middle of housing 1 in a preferably
25 coaxial way, so as to be exposed to gases contained in housing 1 for a length L. Terminals 4, 4' are preferably made up with a conductive material having a low thermal conductivity, such as steel.

In the present embodiment of the invention, the vacuum panel comprises in a known way a discontinuous or porous filling material 5 enclosed between two
30 barrier sheets 6 mutually joined along the edges, for example by means of heat sealing.

Terminals 4, 4' of the sensor are electrically connected to the outside through one or more rheophores 7, 7' arranged between the barrier sheets 6. In particular, rheophores 7, 7' are preferably formed of two conductive bands, both comprising a conductive layer 8 enclosed between two insulating layers 9 mutually joined along the edges, for example by means of heat sealing. The two ends of both conductive bands 7, 7' are further provided with pins 10, 11, the former of which is soldered to a terminal 4 or 4' and the latter is prepared for the connection with external apparatuses.

Referring now also to figure 2, in the present embodiment the conductive bands 7, 7' comprise two insulating layers 9 formed of one or more tapes of polymeric material, in particular a heat sealable tape of high density polyethylene (HDPE) having a thickness comprised between 50 and 100 μm . Insulating layers 9 enclose a conductive layer 8 formed particularly of an aluminum tape having a thickness comprised between 4 and 10 μm . In other embodiments of the present invention layers 9 can be made up with other thermoplastic polymers, such as e.g. polyacrylonitrile (PAN), polyethylene terephthalate (PET), polyvinylchloride (PVC), polypropylene (PP) or other polymers, as well as mixtures and copolymers thereof, while conductive layer 8 can be made up with other conductive metals, such as copper, gold and silver, or with conductive polymers, such as iodine-doped polyacetylene. Conductive layer 8 is inserted between insulating layers 9 by means of colamination, preferably carried out by arranging between layers 8 and 9 an adhesive material, such as epoxidic, cyanoacrylic, polyurethanic, etc. resins. Alternatively, when the currents crossing conductive bands 7, 7' are low, it is possible to produce these latter by joining together two polymeric films acting as insulating layers 9, at least one of which has a metallized surface which is comprised between these films and acts as the conductive layer 8.

In the present embodiment of the invention the conductive bands 7, 7' are arranged between the two barrier sheets 6 of the vacuum panel before they are sealed along their edges. The sealing of the edges of the barrier sheets 6 occurs preferably by means of heat sealing, hence, since these sheets are made up with materials identical, similar or in any case compatible with those used for the

insulating layers 9 of the conductive bands 7, 7', the latter are soldered between the barrier sheets 6, thereby forming a perfect gas-tight joining while avoiding possible current dispersions or short-circuits with the metallic or metallized layer 12 which may occur on the internal surface of the barrier sheets 6.

5 Pins 10, 11 are preferably inserted in a substantially perpendicular way through the conductive bands 7, 7' during the manufacture thereof, so as to pierce layers 8, 9 and to accomplish an electric connection with the conductive layer 8. For this purpose, pins 10, 11 are joined to metallic members, particularly clamps 13, 14 provided with tips crossing the conductive bands 7, 7'. Once the tips of
10 clamps 13, 14 have been inserted into the conductive bands 7, 7', the borders 15, 16 of these latter included between their ends and clamps 13, 14 are folded and heat sealed onto the same bands, so as to enclose and insulate the tips of clamps 13, 14. With this arrangement, pins 10, 11 protrude freely outwards and are at the same time steadily locked along the same plane of the conductive bands 7, 7'.

15 In other embodiments of the present invention, the conductive bands 7, 7' can comprise two or more conductive layers 8 electrically separated from one another, for example arranged side by side between the insulating layers 9 or arranged one on the other and separated by a further insulating layer 9. With this arrangement it is possible to use only one conductive band to electrify the vacuum
20 panel or to send several signals in parallel to electric or electronic devices arranged inside the panel. With these conductive bands, but also with those previously described, it is possible to use terminal boards comprising two or more pins suitable for piercing the ends of the insulating and conductive layers, thus obtaining the electric connection with the electric or electronic devices inside
25 and/or outside the vacuum panel.

Wire 2 is powered through the conductive bands 7, 7' with an external power unit (not shown in the drawings) which supplies a constant current $I = I_2$. When at time $t = 0$ the current starts flowing along wire 2, the latter becomes hot due to the Joule effect. If pressure P of the residual gases in housing 1 is relatively
30 low, in particular lower than 0.1 hecto-Pascal (hPa), the thermal exchange due to these gases is very modest and the temperature of wire 2 increases progressively

from the initial value T_i up to a high final value T_f , which stabilizes when the dissipated thermal power $Q_{f,G}$, depending upon the thermal gradient between wire 2 and the gas mass inside housing 1, is equal to the electric power Q_e supplied from the outside through the conductive bands 7, 7'. If pressure P of the residual gases in housing 1 is relatively high, in particular higher than 1 hPa, when current I_2 starts to flow along wire 2, the mechanisms of the thermal exchange of convective type which keep the final temperature T_f of wire 2 substantially equal to the initial temperature T_i , are immediately established.

Therefore, at low pressures P , wire 2 comes to the stationary conditions absorbing the maximum electric power Q_e and revealing the maximum potential drop ΔV at its ends, since the electrical resistance R of the wire increases at high temperatures T_f . On the contrary, at high pressures P , the electric resistance R and the temperature T_f , and consequently the absorbed electric power Q_e and the potential drop ΔV , are at minimum values.

Figure 3 shows a diagram from which it can be seen how the variation of the potential difference ΔV at the ends of wire 2, measured in stationary conditions, varies according to pressure P of the residual gases present in housing 1, that is, in the vacuum panel.

Figure 4 shows instead a diagram from which it can be seen how the potential difference ΔV measured at the ends of wire 2 develops during the time at a pressure P of the residual gases equal to 0.1 hPa. As it can be seen, the stationary conditions are reached very quickly, in particular in a period of about 5 sec, which thus results to be the time required for measuring the pressure.

In the present embodiment of the invention, wire 2 is powered by an external device capable to supply an electric current I_2 constant in time and to measure at the same time the potential difference ΔV at the ends of wire 2, that is, of pins 11. In this case, the electric power Q_e supplied to wire 2 in stationary conditions results to be a function of pressure P and of the final temperature T_f , since $Q_e = R(T_f) \times I_2^2$ and the temperature T_f reached in stationary conditions depends upon mechanisms of thermal exchange, and thus also upon pressure P .

It is thus clear that, by keeping an electric power Q_e constant or in any case

determinable through the measurement of the potential difference ΔV at the ends of wire 2, that is, of pins 11, it is possible to obtain the pressure P of the residual gases present in the vacuum panel.

Possible changes and/or additions may be made to the embodiment of the
5 invention here described and illustrated without departing from the scope of the same invention.